

**DR. BABASAHEB AMBEDKAR TECHNOLOGICAL UNIVERSITY,  
LONERE – RAIGAD -402 103  
Mid Semester Examination – October - 2017**

**Branch: M.Tech (VLSI)**

**Sem.:- I**

**Subject with Subject Code:- MTVLC102**

**Marks: 20**

**Date:- 09-10-17**

**Time:- 1 Hr.**

**(Marks)**

**Q.No.1 Attempt any one of the following**

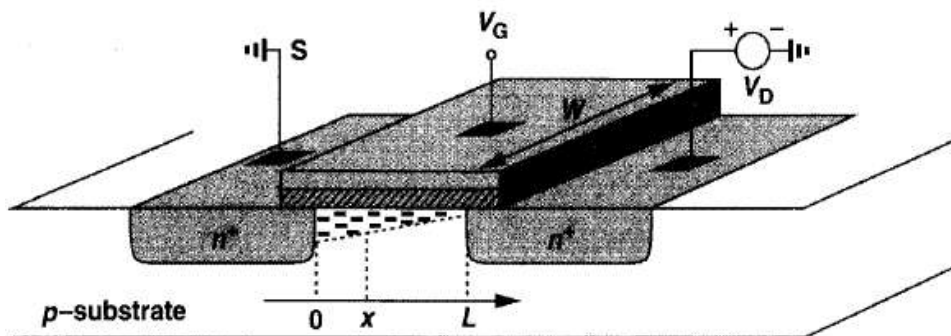
**(08)**

**a.) Derive the equation for drain current in NMOS. Also draw the I/V characteristic.**

**Ans. 1)a)** Consider a semiconductor bar carrying a current  $I$ . If the charge density along the direction of current is  $Q_d$  coulombs per meter and the velocity of the charge is  $v$  meters per second, then

$$I = Q_d \cdot v$$

Consider an NMOS whose source and drain are connected to ground as shown in fig below.



Assuming the onset of inversion occurs at  $V_{GS} = V_{TH}$ , the inversion charge density produced by the gate oxide capacitance is proportional to  $V_{GS} - V_{TH}$ .

For  $V_{GS} \geq V_{TH}$ , any charge placed on the gate must be mirrored by the charge in the channel, yielding a uniform channel charge density (charge per unit length) equal to

$$Q_d = WC_{ox}(V_{GS} - V_{TH})$$

where  $WC_{ox}$  to represent the total capacitance per unit length

Since the channel potential varies from zero at the source to  $V_D$  at the drain, the local voltage difference between the gate and the channel varies from  $V_G$  to  $V_G - V_D$ . Thus, the charge density at a point  $x$  along the channel can be written as

$$Q_d(x) = WC_{ox}[V_{GS} - V(x) - V_{TH}]$$

where  $V(x)$  is the channel potential at  $x$ .

the current is given by

$$I_D = -WC_{ox}[V_{GS} - V(x) - V_{TH}]v$$

where the negative sign indicate the charge carriers are negative and  $v$  denotes the velocity of the electrons in the channel.

For semiconductors,  $v = \mu E$ , where  $\mu$ , is the mobility of charge carriers and  $E$  is the electric field.

Therefore,  $E(x) = -dV/dx$  and representing the mobility of electrons by  $\mu_n$ , we have

$$I_D = WC_{ox}[V_{GS} - V(x) - V_{TH}]\mu_n \frac{dV(x)}{dx}$$

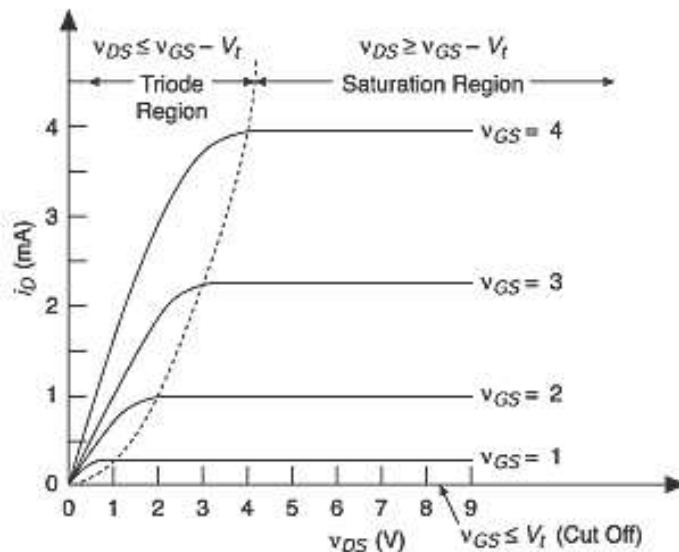
subject to boundary conditions  $V(0) = 0$  and  $V(L) = V_{DS}$ .

Multiplying both sides by  $dV$  and performing integration, we obtain

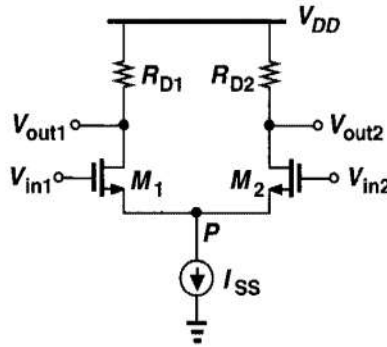
$$\int_{x=0}^L I_D dx = \int_{V=0}^{V_{DS}} WC_{ox}\mu_n[V_{GS} - V(x) - V_{TH}]dV$$

Since  $I_D$  is constant along the channel,

$$I_D = \mu_n C_{ox} \frac{W}{L} \left[ (V_{GS} - V_{TH})V_{DS} - \frac{1}{2}V_{DS}^2 \right]$$



**b.) Derive the differential output current for the figure shown below assuming the circuit is symmetric, M1 and M2 are saturated, and  $\lambda = 0$**



**Ans. 1)b)** For the differential pair

$$V_{out1} = V_{DD} - R_{D1} \cdot I_{D1} \text{ and}$$

$$V_{out2} = V_{DD} - R_{D2} \cdot I_{D2}$$

$$\text{i.e. } V_{out1} - V_{out2} = R_{D2} \cdot I_{D2} - R_{D1} \cdot I_{D1} = R_D (I_{D2} - I_{D1}) \quad \dots \text{if } R_{D2} = R_{D1} = R_D$$

Assuming the circuit is symmetric, M<sub>1</sub> and M<sub>2</sub> are saturated, and  $\lambda = 0$ .

Since the voltage at node P is equal to  $V_{in1} - V_{GS1}$  and  $V_{in2} - V_{GS2}$ ,

$$V_{in1} - V_{in2} = V_{GS1} - V_{GS2}$$

For a square-law device, we have,

$$(V_{GS} - V_{TH})^2 = \frac{I_D}{\frac{1}{2} \mu_n C_{ox} \frac{W}{L}}$$

and, therefore,

$$V_{GS} = \sqrt{\frac{2I_D}{\mu_n C_{ox} \frac{W}{L}}} + V_{TH}$$

$$V_{in1} - V_{in2} = \sqrt{\frac{2I_{D1}}{\mu_n C_{ox} \frac{W}{L}}} - \sqrt{\frac{2I_{D2}}{\mu_n C_{ox} \frac{W}{L}}}$$

Squaring the both the sides of above eq. and recognizing that  $I_{D1} + I_{D2} = I_{SS}$ , we obtain

$$(V_{in1} - V_{in2})^2 = \frac{2}{\mu_n C_{ox} \frac{W}{L}} (I_{SS} - 2\sqrt{I_{D1} I_{D2}})$$

That is,

$$\frac{1}{2}\mu_n C_{ox} \frac{W}{L} (V_{in1} - V_{in2})^2 - I_{SS} = -2\sqrt{I_{D1} I_{D2}}$$

Squaring the two sides again and noting that,

$$4(I_{D1} \cdot I_{D2}) = (I_{D1} + I_{D2})^2 - (I_{D1} - I_{D2})^2 = I_{SS}^2 - (I_{D1} - I_{D2})^2$$

We obtain,

$$(I_{D1} - I_{D2})^2 = -\frac{1}{4} \left( \mu_n C_{ox} \frac{W}{L} \right)^2 (V_{in1} - V_{in2})^4 + I_{SS} \mu_n C_{ox} \frac{W}{L} (V_{in1} - V_{in2})^2$$

Thus,

$$I_{D1} - I_{D2} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{in1} - V_{in2}) \sqrt{\frac{4I_{SS}}{\mu_n C_{ox} \frac{W}{L}} - (V_{in1} - V_{in2})^2}$$

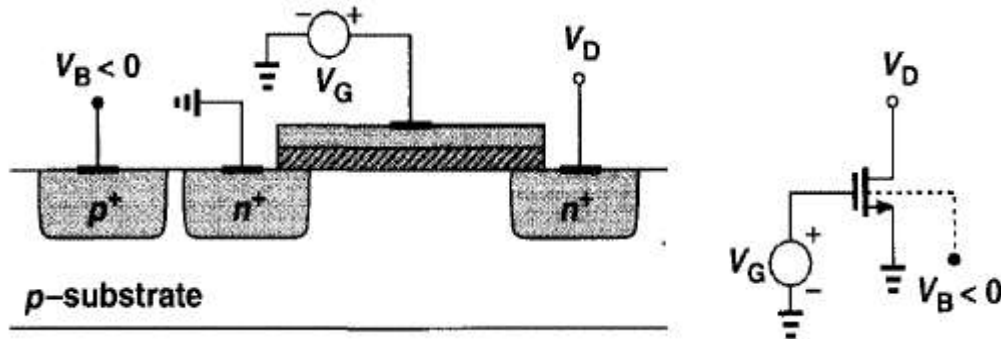
**Q.No. 2 Attempt any three of the following:**

**(12)**

**a.) Explain Body effect in MOSFET**

**Ans 2)a) Body Effect:**

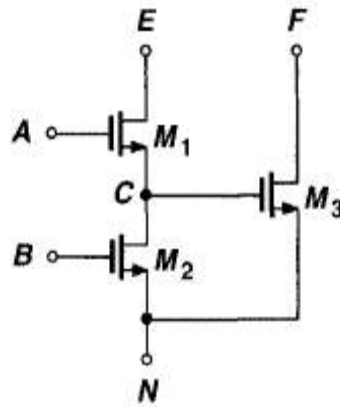
Since the S and D junctions remain reverse-biased, it is surmise that the device continues to operate properly but certain characteristics may change.



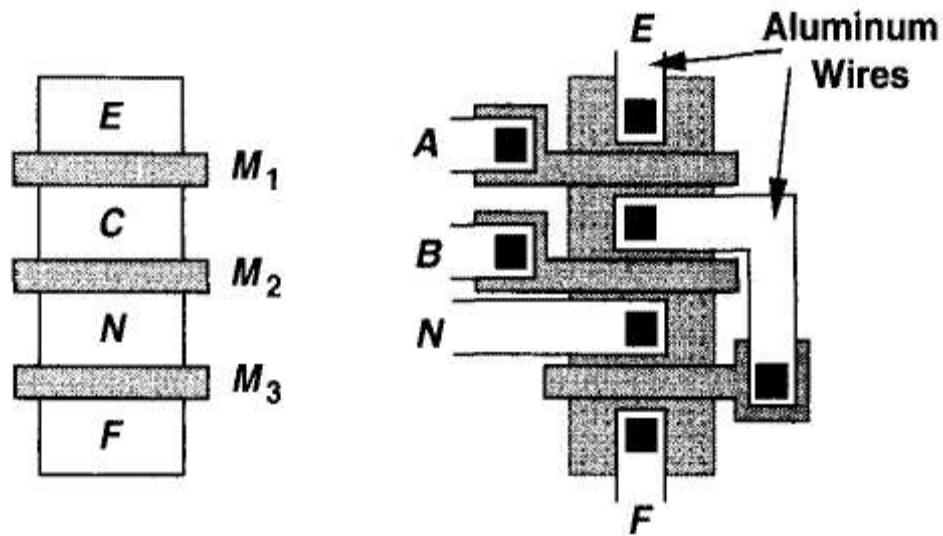
**Figure :** NMOS device with negative bulk voltage

To understand the effect, suppose  $V_S = V_D = 0$ , and  $V_G$  is somewhat less than  $V_{TH}$  so that a depletion region is formed under the gate but no inversion layer exists. As  $V_B$  becomes more negative, more holes are attracted to the substrate connection, leaving a larger negative charge behind, i.e, the depletion region becomes wider. Also the threshold voltage is a function of the total charge in the depletion region because the gate charge must mirror  $Q_d$  before an inversion layer is formed. Thus, as  $V_B$  drops and  $Q_d$  increases,  $V_{TH}$  also increases. This is called the "body effect" or the "backgate effect."

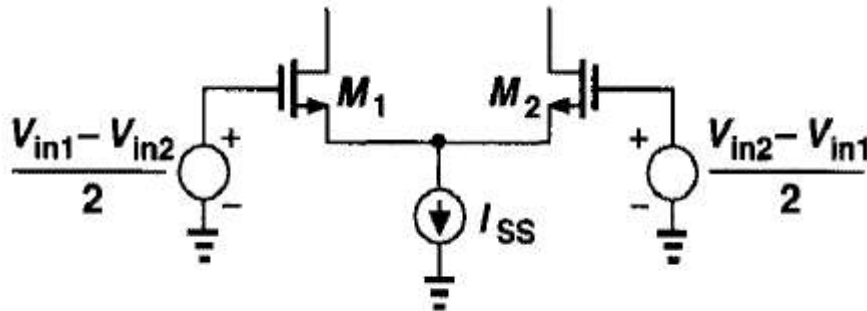
b.) Draw the layout of the circuit shown in Fig



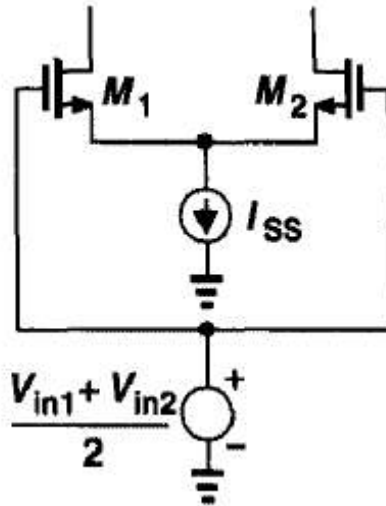
Ans 2)b)



c.) In the circuit of shown below, calculate  $V_x$  and  $V_y$  if  $V_{in1} \neq -V_{in2}$  and  $\lambda \neq 0$ .



Ans 2)c) Simplifying the given circuit,



For differential-mode operation, from the above circuit we have,

$$V_X = -g_m(R_D \parallel r_{O1}) \frac{V_{in1} - V_{in2}}{2}$$

$$V_Y = -g_m(R_D \parallel r_{O2}) \frac{V_{in2} - V_{in1}}{2}.$$

$$V_X - V_Y = -g_m(R_D \parallel r_O)(V_{in1} - V_{in2}),$$

**d.) Explain advantage of current mirror.**

**Ans 2)d)** The advantages of a current mirror are:

1. low input impedance makes the input current insensitive to the output impedance of the input source
2. high output impedance makes the output current insensitive to the impedance of the output load
3. inversion of sources to sinks or sinks to sources
4. accurate gain
5. shifts between different power rails.